

Investigation of mechanical properties and abrasive assisted electrochemical machining parameters on Al6061-10%TiB₂-3%Gr hybrid ceramic composite

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This research paper investigates mechanical, morphological behavior of Al6061-3%Gr, Al6061-10%TiB₂, Al6061-10%TiB₂-3%Gr and optimizes input machining parameters in abrasive assisted and straight electro chemical machining. The Hybrid ceramic composite (HCC) are reinforced with TiB₂ and Graphite. The composites are fabricated by stir casting method to achieved good mechanical property and wear resistance. This hybrid composite are highly suitable material for automobile and aerospace components. ECM is an excellent way to produce micro components with special features and this fabrication method is used for biomedical applications. Machining of HCC is very serious problems due to its hardness. The ECM is a very complex process in practice. The quality of production mainly depends on the input machining parameters. The economical and high quality of micro drill on HCC is achieved by controlling machining parameters like current, voltage, electrolyte concentration, feed rate, gap between the tool and work. Performance of abrasive assisted ECMM and straight ECMM process in terms of maximum material removal rate and minimum overcut were analysed. The maximum material removal rate is acquired through abrasive assisted ECMM process.

Keywords: Al6061-10%TiB₂-3%Gr, Stir Casting, Electrochemical Machining, Over Cut, Material Removal Rate.

Introduction

The Hybrid ceramic composite fabrication through liquid stir casting routine is much admired technique because of its exclusive advantages [1-2]. Al-TiB₂ composite is one of the outstanding composite in mechanical sectors where light weight, superior mechanical properties and better wear resistance are major deliberation especially in automobile, aeronautical applications [3]. Micro slots and holes produced in micro products with complex features in ECMM technology have been effectively adapted. Wide- range of desirable research work is required in the region of machining parameter and tool design [4]. The micro machining in HCC is very complicated process because of the hard reinforcement particles present in the matrix. Due to hard particles present in the main matrix the micro drilling HCC is a difficult task for production engineers. The majority of recent literatures deals in terms of tool life, quality of drilled hole, and surface roughness during micro drilling in HCC [5]. The micro ECM is extremely difficult, so it is not easy to desire the most favorable machining parameters for improving the production superiority. The optimization of process parameters is necessary for the understanding of a higher productivity with desired quality, which is the primary endurance in today's

forceful market circumstances. Most favorable quality of micro hole in ECM is able to generate through combinational control of different process parameters [6]. Graphite reinforcement particles have excellent lubricates property used in an extensive range of applications in aluminium composite materials. So this reinforcement composite material is used to construct components in definite mechanical and morphological behaviors, and enormous wear resistance property such as engine cylinder liner pistons and piston rings and bearing [7-8].

Many of literatures authenticate that there is no clear work is carried out on Al6061+TiB₂+Gr composite material fabricated in liquid phase route. In this research Al6061+10%TiB₂+3%Gr composite material is fabricated by and analysis of the mechanical and morphological behaviors of that hybrid composite is done. The chemical composition of Al6061, Gr and TiB₂ are shown in Table 1-3 respectively. This research work is generally focuses on mechanical and morphological behavior of Al6061-10%TiB₂-3%Gr hybrid composite. The investigation of the ECMM machining parameters are analysed for producing the high quality micro drill on Al6061-10%TiB₂-3%Gr hybrid composite.

Methodology

By using stir casting method Al6061-3%Gr, Al6061-10%TiB₂ and Al6061-10%TiB₂-3%Gr aluminium hybrid composites are fabricated [9-10]. The mechanical and

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Table 1. Composition of Al 6061

Elements	Ni	Cu	Mn	Mg	Ti	Pb	Zn	Fe	Si	Cr	Aluminium
%weight	0.05	0.24	0.139	0.802	0.15	0.24	0.25	0.7	0.43	0.25	Balance

Table 2. Chemical composition of Gr

Elements	Fe	S	C
%weight	0.5	0.1	95.00

Table 3. Chemical composition of TiB₂

Elements	Fe	C	Ti	B	O	N
%weight	0.09	0.25	67.6	31.04	0.45	0.26

morphological behaviors of obtained hybrid composite were compared with Al6061 [11]. These composites are investigated for its machining parameters using ECMM for producing the high quality micro drill on Al6061-10%TiB₂-3%Gr hybrid composite.

Al6061+10Wt%TiB₂+3Wt% Gr composite materials fabricated by liquid phase route (stir casting method). Initially Al6061 material was melted for 60 minutes in a muffle furnace at 700 °C. The reinforcement particles TiB₂ and Graphite (Gr) particles are primarily preheated at 850 °C for 60 minutes for oxidation progression. The Gr reinforcement particles are added into the molten metal (25-30 μm) and the furnace temperature is maintained at 750 °C. The TiB₂ particles are fed into the molten liquid at 0.01Kg/min while maintaining the stirring rate at 400 rpm in the whole time process. The Al6061+10Wt%TiB₂ and Al6061+3Wt% Gr composites are produced in same approach [12-14].

The potential strength of tensile, yield, ultimate and ductility were measured as per ASTM E8M standard for every composite. Brinell hardness test was carried out in every sample with 250 kg load with 5 mm diameter steel ball indenter as per ASTM E10 standard for every composite. From the above test results normal value has been taken and graph was plotted as per the average value. Microstructure studies carried out in every specimen in polishing and etched route [15].

Formation of high quality micro holes in micro products is complex nature. Electro chemical machining is excellent way to produce the micro holes. It was very difficult to achieve good surface finish with high precision of dimension [3, 16]. Abrasive assisted electro chemical micro machining is excellent way to achieve maximum MRR, good surface finish with high precision of dimension. Based on the beginning experimental trial results the levels are recognized. The dimensions of work material 50×50×0.4 mm obtained through wire cut EDM. The experimental setup used in this research work is shown in Fig. 1. The experimental system used for electrochemical machining process is presented in Table 4. The input process parameter and its levels used in this research work are presented in Table 5. Based on the previous literatures the process parameters

**Fig. 1.** Experimental setup.**Table 4.** ECMM Experimental system

ECMM Experimental System	
AL6061+10wt%TiB ₂ +3wt%Gr (50X50X0.4 mm ³)	Work piece
Sodium Nitrate	Electrolyte concentration
Silicon carbide particles (50 μm)	Abrasive medium
500 μm Cylindrical bronze Tool	Electrode

Table 5. Process parameters and its levels

ECMM Input Process Parameters				
Symbol	Description of Factors	Level -1	Level -2	Level -3
E	Electrolyte Flow rate (g/L)	20	25	30
V	Voltage (V)	10	12	14
F	Frequency (Hz)	30	40	50
-	Gap (mm)	0.1	0.1	0.1
-	Current (A)	0.8	0.8	0.8

are selected. This is also analysed with the industrialists working in this area and the levels of the process parameters are selected. Micro drilling of HCC is performed in ECM and abrasive assisted ECM. The responses selected are material removal rate and overcut. Design of experiment is used to conduct the experiments and L27 orthogonal array is performed and the composition of the process parameters for conducting each run is designed using Minitab software. The experimental data comprising the 27 experiments and measured responses are recorded in Table 6.

Result and Discussion

Mechanical properties

The hardness of Al6061 and its hybrid composites

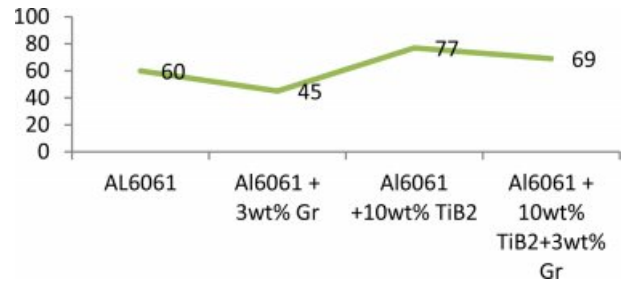
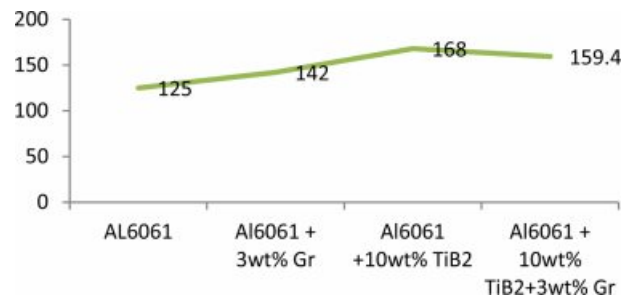
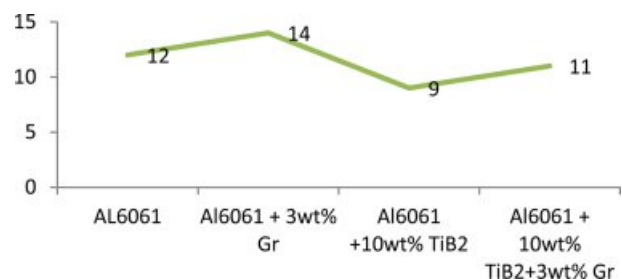
Table 6. Experimental data

Trial No	ECMM Process Parameters	Experimental Result AECM		Experimental Result ECM	
		MRR (mg/min)	OC (μm)	MRR (mg/min)	OC (μm)
1	V1,E3,F1	0.293	160.14	0.253	159.98
2	V1,E3,F2	0.245	188.03	0.185	187.83
3	V1,E3,F3	0.275	190.29	0.213	190.09
4	V2,E3,F1	0.306	110.63	0.245	110.43
5	V2,E3,F2	0.218	172.28	0.155	172.08
6	V2,E3,F3	0.202	96.95	0.141	96.75
7	V3,E3,F1	0.234	161.45	0.178	161.25
8	V3,E3,F2	0.305	171.26	0.144	171.06
9	V3,E3,F3	0.286	146.56	0.225	146.36
10	V1,E2,F1	0.305	162.45	0.248	162.25
11	V1,E2,F2	0.285	141.43	0.221	141.23
12	V1,E2,F3	0.248	158.65	0.178	158.45
13	V2,E2,F1	0.138	133.42	0.064	133.22
14	V2,E2,F2	0.335	153.04	0.275	153.04
15	V2,E2,F3	0.164	170.65	0.102	170.35
16	V3,E2,F1	0.156	154.26	0.095	154.06
17	V3,E2,F2	0.135	232.56	0.074	232.36
18	V3,E2,F3	0.146	182.31	0.089	182.11
19	V1,E1,F1	0.134	227.15	0.065	227.05
20	V1,E1,F2	0.149	182.35	0.088	182.15
21	V1,E1,F3	0.245	156.62	0.185	156.42
22	V2,E1,F1	0.221	144.35	0.154	144.15
23	V2,E1,F2	0.138	184.21	0.089	184.01
24	V2,E1,F3	0.225	143.85	0.171	143.55
25	V3,E1,F1	0.105	177.82	0.054	177.52
26	V3,E1,F2	0.178	203.27	0.118	202.87
27	V3,E1,F3	0.149	184.18	0.095	184.01

containing 3 wt% Gr, 10 wt% TiB₂ are evaluated using Brinell hardness tester. From Fig. 2, it is observed that adding the Gr particles into the Al6061 the hardness nature is decreased. Adding TiB₂ particles into the AL6061 hardness value is 17% increased compare with AL6061. From Fig. 3, it is observed that the addition of TiB₂, Gr reinforcement particles into the main matrix increases the ultimate tensile strength gradually. From Fig. 4, it is noted that the % elongation and the ductile behavior was increased by the addition of Gr particles into AL6061. The addition of Gr particles composite material becomes soft, ductile and increasing lubricating behavior. The TiB₂ reinforcement particles added into the AL6061 which resists course dislocations causes decreased ductile behavior. The mechanical properties

Table 7. Mechanical properties

Specimen	Brinell Hardness number	Tensile Strength (MPa)	% Elongation
AL6061	60	125	12
Al6061 + 3wt% Gr	45	142	14
Al6061 +10wt% TiB ₂	77	168	9
Al6061 + 10wt% TiB ₂ +3wt% Gr	69	159.4	11

**Fig. 2.** Brinell Hardness.**Fig. 3.** Tensile strength.**Fig. 4.** % Elongation.

for various HCC compositions are presented in Table 7.

Fractography

The reinforcement particles circulation is homogeneous and there is no porosity, cracks formed. Figs. 5(a) to (d) represents the scanning electron microscopic images of the HCC specimen used in this research work. Fig. 5(a) represents the image of AL6061. The reinforcement particles circulation is homogeneous and there is no porosity, cracks formed. The wt%TiB₂, wt%Gr particles is clearly exposed in the microphotographs. Fig. 5(b) represents the image of HCC of Al6061-3%Gr. It is observed that the Graphite is distributed evenly and provides good lubrication effects for the specimen.

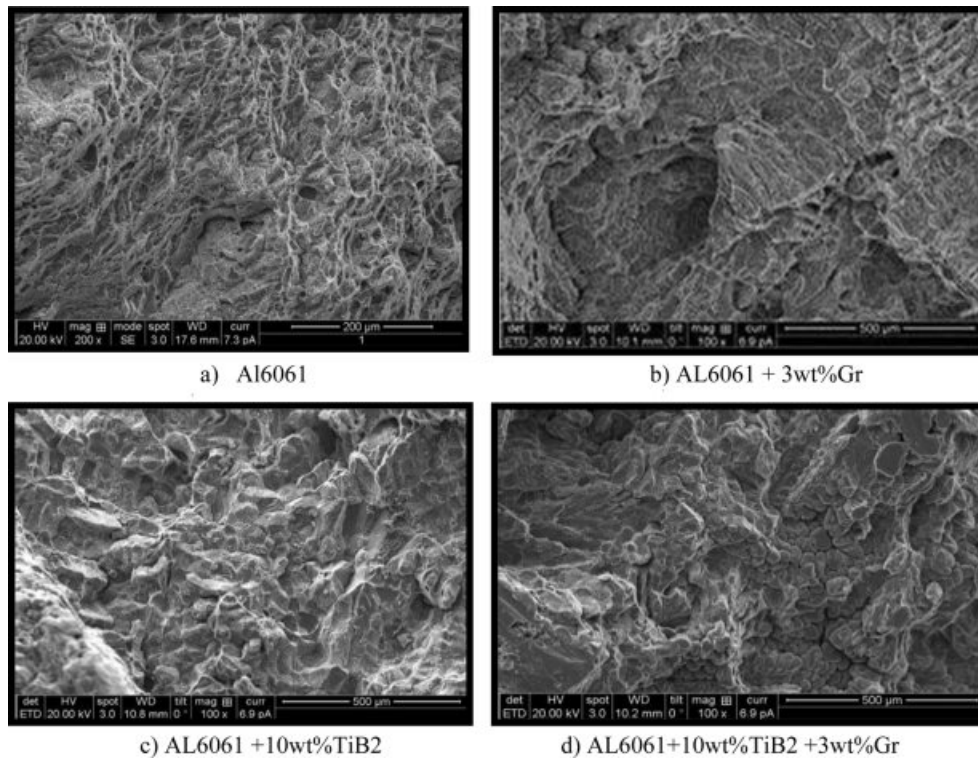


Fig. 5. SEM Images.

Fig. 5(c) represents the image of HCC of AL6061-3%Gr-10%TiB₂, which describes the distribution of the reinforcing elements – Graphite, TiB₂ in the metal matrix and is observed that the reinforcing elements are distributed evenly and provides higher strength. Fig. 5(d) represents the image of AL6061-3%Gr-10%TiB₂ and composition of all the elements present in the HCC is shown and they are distributed evenly. This image also reveals that the cracked surfaces defines the ductile fracture including of frequent dimples over whole surfaces of base metal. When addition of Gr reinforced into the base metal shows hairline fracture with less amounts of dimples on the surface. The addition of TiB₂ into the base metal shows the ductile and brittle fracture nature.

Taguchi Technique on Micro drilling process on AL6061-10%TiB₂ - 3%Gr hybrid composite

The quality micro holes is produced by electro chemical

micro machining setup and as well as abrasive assisted electro chemical micro machining setup through controlling of initial machining parameters. The drilling process is carried out twice in each process parameter setup. Machining time, overcut and material removal rate is obtained in each and every experiment level. The responses of each process parameters are obtained by Taguchi method. L₂₇ OA is used to conduct 27 experiments and the responses are recorded and analysed.

Table 8 and Table 9 represents the response table Response table for micro drilling process on AL6061-10%TiB₂ - 3%Gr hybrid composite in ECM and AECM respectively. Fig. 6 and Fig. 7 represents the main effects plots for the SN ratios for material removal rate and overcut respectively. Fig. 8 and Fig. 9 represents the interaction effect of the process parameters over the responses for material removal rate and overcut respectively. It is observed that the material removal

Table 8. Response table for micro drilling process on AL6061-10%TiB₂ - 3%Gr hybrid composite in ECM

Electro chemical micro drilling process						
Level	Voltage (V)		Electrolyte concentration (E)		Frequency (Hz)	
	MRR	OC	MRR	OC	MRR	OC
1	-10.32	-43.73	-12.61	-43.73	-11.16	-42.852
2	-11.17	-41.86	-11.23	-43.21	-11.18	-43.761
3	-11.96	-43.83	-9.57	-42.39	-11.125	-42.618
Delta	1.314	2.06	2.923	1.58	0.172	1.32
Rank	3	3	1	2	2	1

Table 9. Response table for micro drilling process on Al6061-10%TiB₂ - 3%Gr hybrid composite in AECM

Abrasive Assisted Electro chemical micro machining process						
Level	Voltage (V)		Electrolyte concentration (E)		Frequency (Hz)	
	MRR	OC	MRR	OC	MRR	OC
1	-10.37	-43.74	-12.67	-43.79	-11.23	-42.84
2	-11.25	-41.91	-11.22	-43.17	-11.21	-43.78
3	-12.12	-43.85	-9.55	-9.61	-11.234	-42.62
Delta	1.428	2.07	3.013	1.53	0.195	1.27
Rank	3	3	1	2	2	1

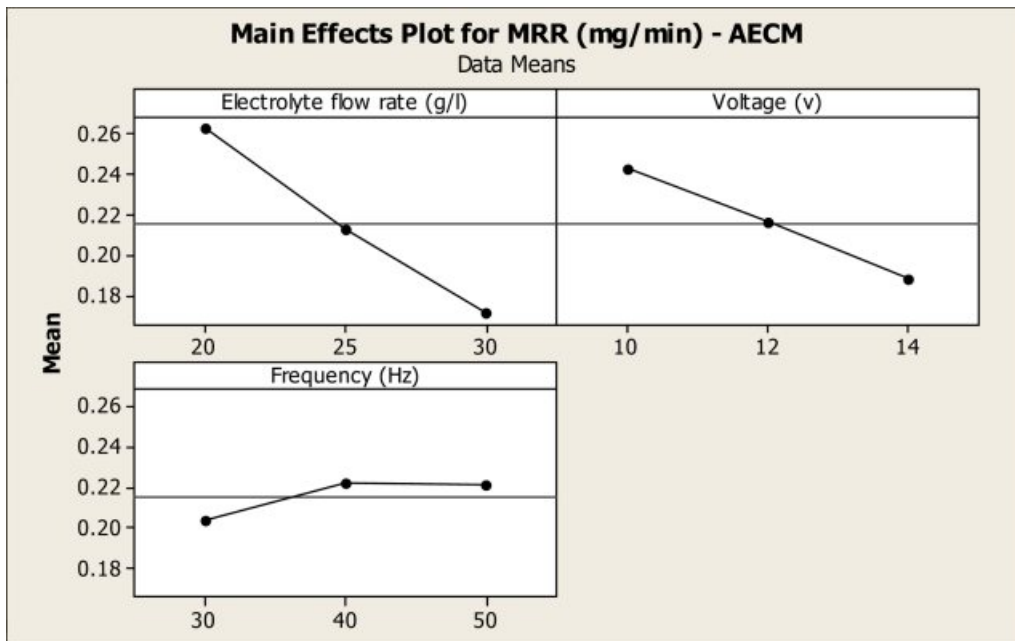


Fig. 6. Main Effects plot for SN ratios of MRR.

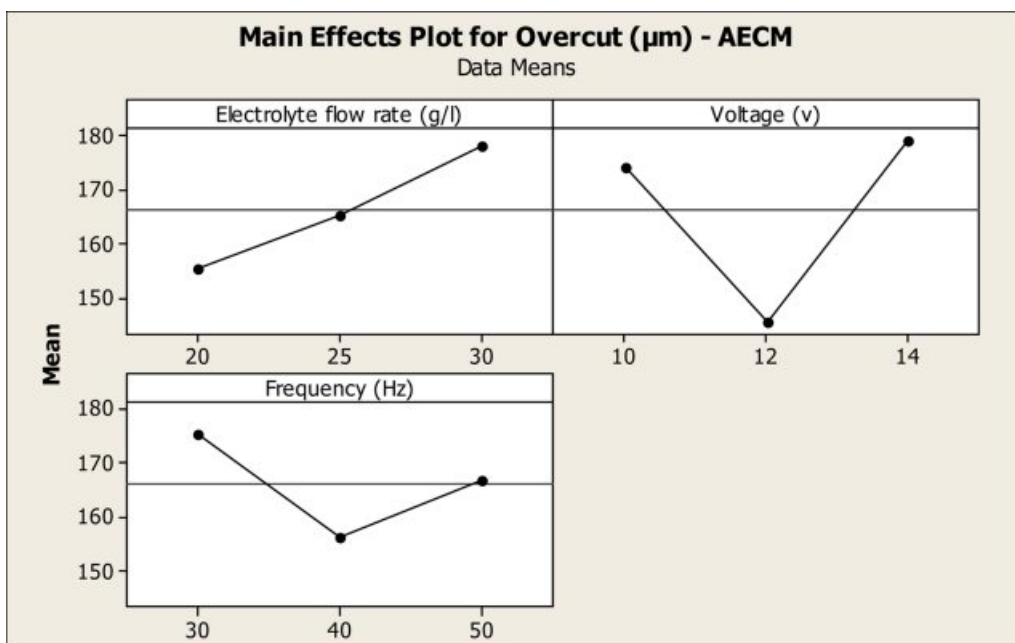


Fig. 7. Main Effects plot for SN ratios of Overcut.

rate shows a very little change with frequency, whereas when the voltage increases there is a decrease in material removal rate and it is vice versa with respect to the electrolyte concentration. From the main effects plots and the interactions plot, it is observed that the electrolyte concentration is the most influencing parameter and it is followed by frequency and voltage. Similarly in the overcut, it is observed that the frequency is the most influencing parameter and it is followed by electrolyte concentration and voltage.

Similarly, it is observed that overcut increases with increase in electrolyte concentration whereas the voltage and frequency finds a rapid change. The maximum material removal rate is identified at 40 Hz, 30 g/L, 10 V and the smallest amount of overcut is identified at 50 Hz, 30 g/L, 12 V. Interaction plots explain MRR and OC interactions on each level of the process parameters. The most favorable level of MRR is identified at categorization of medium frequency, higher electrolyte concentration and minimum voltage, and least amount

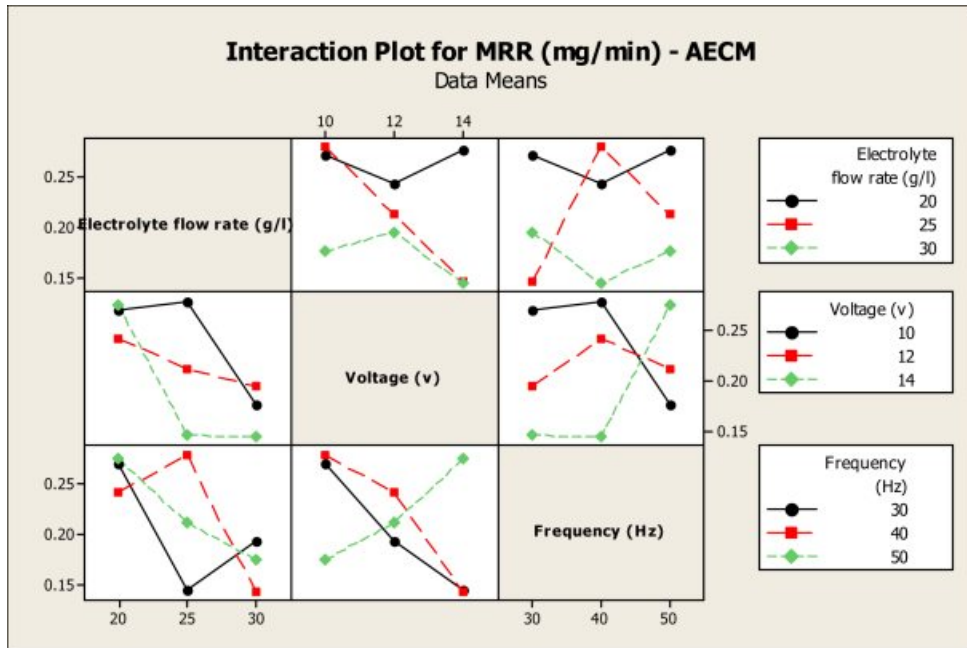


Fig. 8. Interaction effect for SN ratios of MRR.

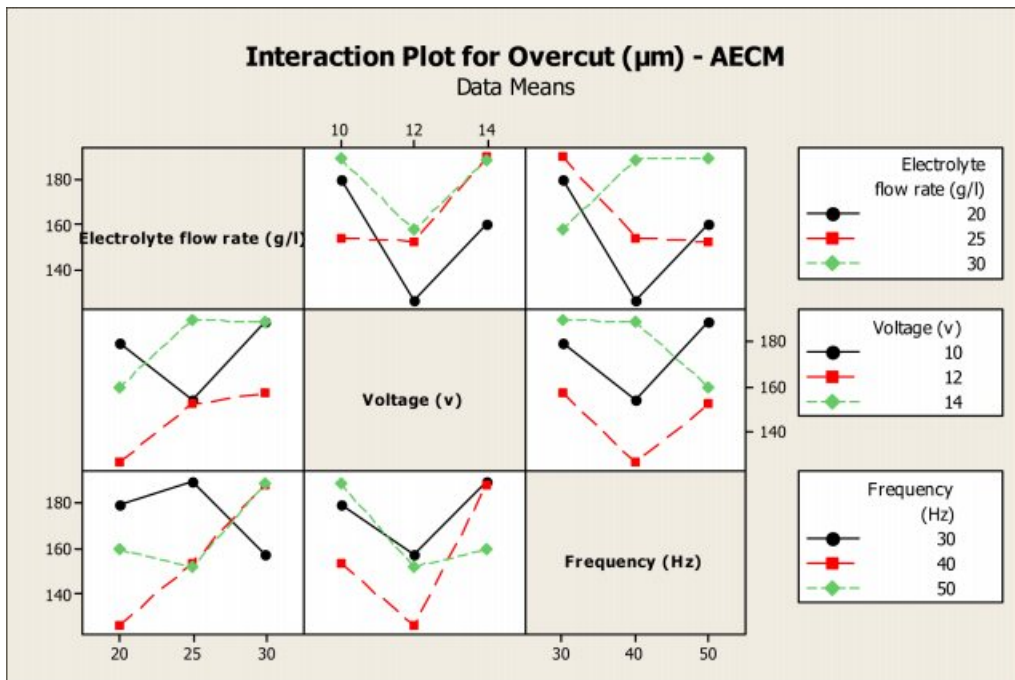


Fig. 9. Interaction effect for SN ratios of Overcut.

of Over Cut is found at combination sequence of maximum frequency, minimum electrolyte concentration and medium voltage. The residual plots for material removal rate and overcut are shown in Fig. 10 and Fig.

11 respectively. In residual graphs, all the points lies very close to the central median line and in between the upper median line and lower median line. This infers that the mathematical equation are satisfactory

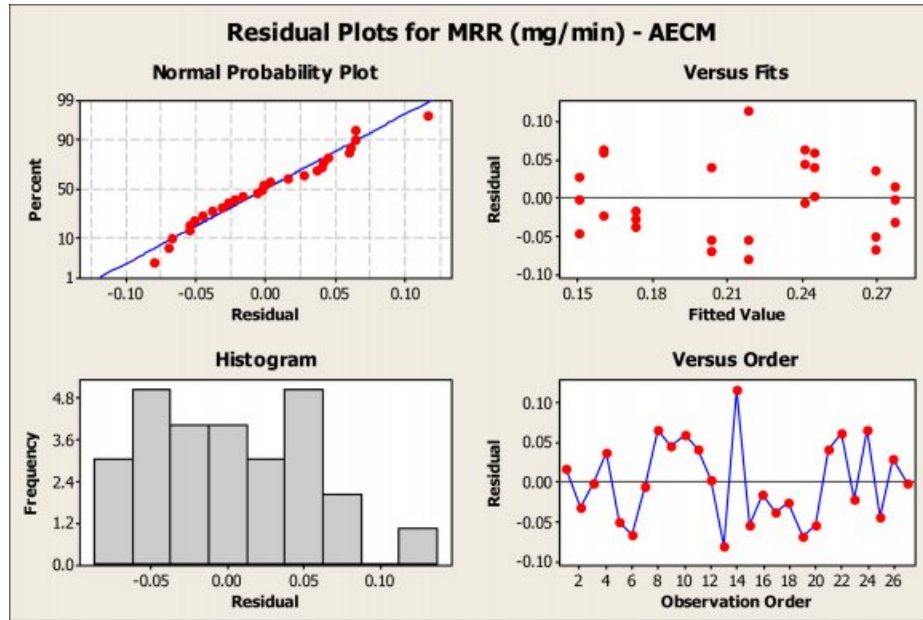


Fig. 10. Residual plots for MRR.

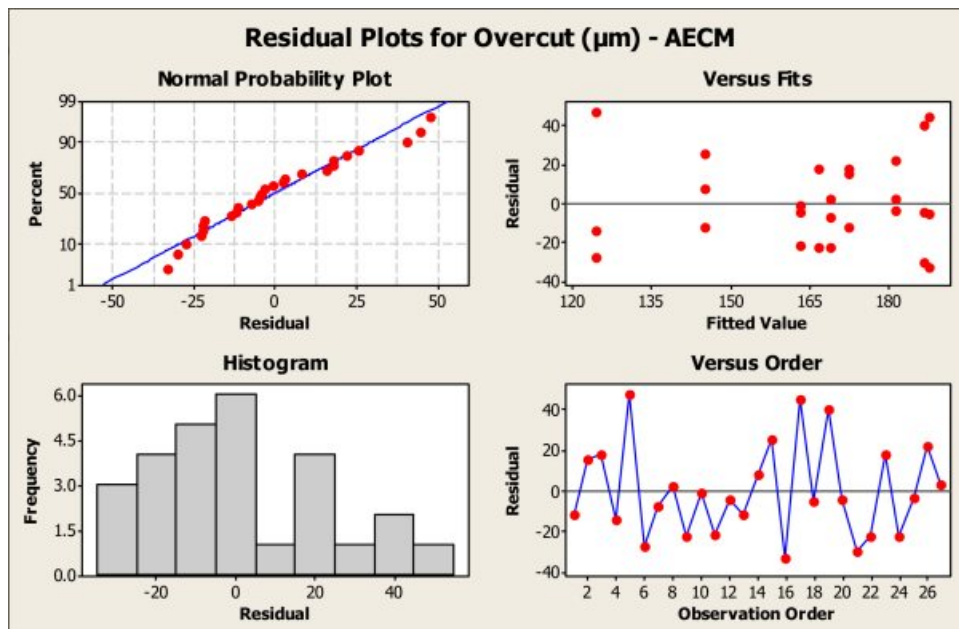


Fig. 11. Residual plots for Overcut.

Table 10. Validation

Process Parameters		MRR (mg/min)		Process Parameters		Over Cut (µ m)		
		AECM	ECM			AECM	ECM	
Initial level	V1E1F1	0.134	0.065	V1E1F1	227.15	227.05		
Experimental level	V1E3F2	0.245	0.185	V2E3F3	96.95	96.75		
% of Improvement		45.3%	64.9%			57.31%	57.38%	
% of MRR Improvement		In AECM process 24.45% is increased compare with ECM process						

and the results are within the acceptable limit. Validation is conducted for material removal rate and overcut for HCC drilled in ECM and AECM and it is observed the material removal rate is increased to 45.3% in AECM and 64.9% in ECM, similarly the overcut is increased to 57.31% in AECM and 57.38% in ECM. Comparatively it is observed that there is an increase of 24.45% in AECM process when compared to ECM process. The validation results are given in Table 10.

Conclusion

In this work, Al6061+3Wt%Gr, Al6061+10Wt%TiB₂ and Al6061+10Wt%TiB₂+3Wt%Gr composites through liquid metallurgy route was prepared. Micro structure shows the reinforcement particles was homogeneously distributed in the composite. In addition of graphite particles into the Al6061 matrix ultimate strength of the composite material is increased. Introducing 10Wt%TiB₂ particles into the Al6061 base material increases the value of hardness and the UTS of composite. Introducing 10Wt%TiB₂ and 3Wt%Gr particles into the Al6061 base material, it increases the value of UTS compared with Al6061-10Wt%TiB₂ and Al6061-3Wt%Gr composites. The ductility value of hybrid composites Al6061+10Wt%TiB₂+3Wt%Gr was higher than Al6061+10Wt%TiB₂ composites but less when compared to Al6061+3Wt%Gr composites. The hardness value of Al6061+10Wt%TiB₂+3Wt%Gr hybrid composites was more than Al6061+3Wt%Gr composites but the hardness value is very near compared to Al6061+10Wt%TiB₂ composites. In ECM micro drilling process the rate of MRR is improved upto 64.9% and OC is recovered upto 57.38% compared to initial levels of machining parameters. The Maximum MRR was achieved at 30 g/L electrolyte concentration, 40 Hz frequency, 10 V machining voltage and minimum overcut obtained at 30 g/L electrolyte concentration, 50 Hz frequency, 12 V machining voltage. The MRR is pretentious as a result of machining voltage and frequency and Over cut is is pretentious as a result of the electrolyte concentration

and Frequency. Based on validation result the material removal rate of abrasive electrochemical machining process is improved upto 24.45% compared with straight ECM process, this is because in AECM process MRR is produced by combination effect of anodic dissolution and mechanical abrasion. Al6061+10Wt%TiB₂+3Wt%Gr crossbreed composites were one of the encouraged commercial materials in the engineering aspects of composites.

References

1. J. Hashim, L. Looney, and M.S.J. Hashmi, *J. Mater. Process. Technol.* 92 (1999) 1-7.
2. J. Hashim, L. Looney, and M.S.J. Hashmi, *J. Mater. Process. Technol.* 123[2] (2002) 258-263.
3. Q. Cai, Y. Liu, Z. Ma, L. Yu, J. Xiong, and H. Li, *J. Alloys Compd.* 586 (2014) 78-84.
4. P. Satishkumar, N. Natarajan, S. Dharmalingam, and P. Pitchandi, *Int. J. Heavy Veh. Syst.* 25[3-4] (2018) 430-441.
5. M.M.K. Reddy, *Int. J. Mech. Eng. Appl.* 1[4] (2013) 78-86.
6. A. RiazAhamed, P. Asokan, S. Aravindan, and M.K. Prakash, *Int. J. Adv. Manuf. Technol.* 49[9-12] (2010) 871-877.
7. M. Roy, B. Venkataraman, V. Bhanuprasad, Y.R. Mahajan, and G. Sundararajan, *Metall. Trans. A* 23[10] (1992) 2833-2847.
8. R. Thirumalai, J. Senthilkumar, P. Selvarani, R.M. Arunachalam, and K.M. Senthilkumar, *Aust. J. Mech. Eng.* 10[2] (2012) 157-168.
9. N. Natarajan and R.M. Arunachalam, *NISCAIR Online Periodicals Repository* 70[07] (2011) 500-505.
10. Y. Pazhouhanfar and B. Eghbali, *Mater. Sci. Eng. A* 710 (2018) 172-180.
11. S. Suresh, N.S.V. Moorthi, S.C. Vettivel, and N. Selvakumar, *Mater. Design* 59 (2014) 383-396.
12. S. Murugan, T. Senthil, and P.D. Rajan, *J. Metall. Mater. Sci.* 60[2] (2018) 73-78.
13. D. Dey, A. Bhowmik, and A. Biswas, *J. Comp. Mater.* 55[14] (2021) 1979-1991.
14. M. Paidpilli, G.K. Gupta, and A. Upadhyaya, *J. Comp. Mater.* 53[9] (2019) 1181-1195.
15. H. R. Ezatpour, S. A. Sajjadi, M. H. Sabzevar, and Y. Huang, *Mater. Design* 55 (2014) 921-928.
16. Bhandare, Rajeshkumar, Gangaram, Parshuram, and M. Sonawane, *Int. J. Eng. Adv. Technol.* 3[3] (2013) 61-65.